

Characteristics of Thermally Sprayed NiCrBSi Coatings before and after Electromagnetic Induction Remelting Process

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Abstract: Active mechanical components that work in highly aggressive environments require protection against premature deterioration and, at the same time, it is necessary to ensure a long lifespan. In order to achieve these important features, a protective coating can be added. In this work, a NiCrBSi self-fluxing alloy powder was employed, as feedstock material. The coating was deposited by means of oxyacetylene flame spraying process, achieving a thickness of approximately 1000 μm and exhibiting a high degree of porosity and a weak mechanical adhesion to the substrate. To improve these characteristics, a remelting process using high frequency currents was applied. After the remelting process, the porosity decreased, from an initial value of approximately 15%, to a final value under 3%. Although the microhardness values did not change significantly, both wear-rate and corrosion behavior improvement, after the electromagnetic remelting, was observed.

Keywords: NiCrBSi; self-fluxing alloy; flame spraying; inductive remelting process; pin-on-disk; microhardness; corrosion behavior

1 Introduction

Parts that work in highly aggressive environments must be protected against premature deterioration, corrosion and wear and at the same time, it is strongly

necessary to ensure a long lifetime of the components. Thermally sprayed coatings offer a practical and economical solution to improve corrosion and wear resistance on these types of elements [1, 2]. Nickel based hard materials, such as NiCrBSi family; have been recently used in industries where corrosion and wear resistance is strongly required like: paper, petrol, hot working punches or heat exchangers [3-6]. Many studies showed that these coatings are an alternative for hard chromium coatings, which are harmful to the environment [7].

Thermal spraying is regarded as a suitable technique of coating components, in which a molten or semi-molten material is sprayed on a surface, which is commonly degreased and sand-blasted in advance. The technology can provide coatings thicknesses from a few micrometers to a few millimeters, depending on the used material and the applied coating technique. The majority of coating techniques which belong to thermal spraying use a powder as raw material. For example, high velocity oxygen fuel (HVOF) process can be used in order to obtain reduced porosity for the as sprayed coatings [8]. Another combustion process is flame deposition, using oxyacetylene. This process is also known as LVOF (low velocity oxygen fuel), which is generally used to repair damaged parts [9].

Currently, a great deal of conventional and expensive processes are studied and employed in order to deposit NiCrBSi powder on various substrates. An attempt of HVOF deposition of NiCrBSi coatings with a high content of Cr (14.5%) and Fe (4.5%) on a low alloyed steel substrate was successfully performed by L. Vieira *et al.* Though, the microscopic investigations revealed cracks at the coating-substrate interface, with possible peeling, it showed as well a high degree of micro porosity in the coating [10]. Another research in this field was performed by a team from the Netherlands, which tried to apply a coating using a similar type of powder, but with a higher Cr content (16.5%) by means of laser deposition process. The obtained NiCrBSi coating exhibited significant cracks and possessed high concentration of internal stress, although a pre-treatment of the substrate at 500°C was applied [11].

Therefore, this work aims to deposit the self-fluxing alloy NiCrBSi using a two-step deposition process. Firstly, an inexpensive deposition technique is considered (LVOF). The thermal spraying method consists of melting and propelling particles by a flame, towards a substrate, in order to form the NiCrBSi coating on a EN S355 J2 steel. Secondly, to solve the initial problems regarding the increased porosity, minimize the induced microcracks and to investigate the corrosion and wear behavior, flame remelting and high frequency current remelting was performed.

2 Experimental Procedure

2.1 Materials

The powder N330-FS6 delivered by the British company LSN Diffusion used in this study is a nickel based alloy produced through water atomizing process. The chemical composition of the powder can be seen in Table 1.

Table 1
The chemical composition of the NiCrBSi employed powder

Powder	Ni [%]	Cr [%]	B [%]	Si [%]	Fe [%]
N330-FS6	bal.	6	1	1.5	0.3

Employing this technique, spherical powder particles with small internal porosities and excellent flowability are produced [12]. In Figure 1, the morphology of the NiCrBSi powder used as a raw material is presented.

The elements Cr and B, which are present in the chemical composition of the powder increase the corrosion and respective the wear resistance, due to the fact that they are carbide-forming elements. Moreover, the presence of Si and B favors the wettability and deoxidation during the remelting process [13]. Additionally, these elements decrease the rate of un-remelted particles after the deposition process and after the heat treatment [14]. As substrate material, a non-alloyed EN S355 J2 quality steel was chosen.

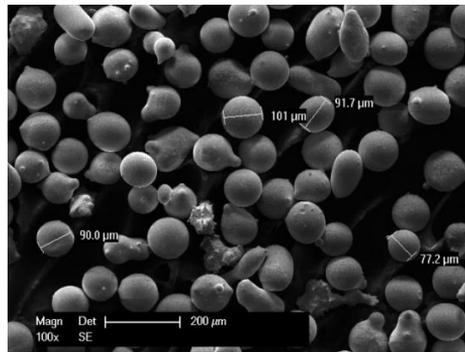


Figure 1

SEM micrograph of NiCrBSi gas atomized water collected powder

2.2 Sample Preparation

The NiCrBSi powder was sprayed using a LVOF technique, applying an oxidant flame, produced by a mix of gases, oxygen and acetylene. The coatings were deposited by the company Karl-Schumacher GmbH, Germany using a flame spraying gun produced by Metatherm, Germany. The geometry of the substrate was a cylindrical workpiece with a diameter of 70 mm and a length of 50 mm. Specimen degreasing and activation before deposition was done with alcohol followed by sandblasting creating the conditions for a good mechanical hooking of the splats. The sample was fixed in a lathe machine and the deposition process was performed. The spraying gun was advanced with a constant feed rate until a thickness of approximately 1 mm was achieved.

After the spraying process, the sample was subjected to two different remelting processes. The first sample was remelted by flame using an oxyacetylene gas process with a neutral stoichiometry. The second sample was remelted using an EKOHEAT 200/30 induction heater manufactured by Ambrell, The Netherlands. The induction heating unit requires from 15 kHz to 40 kHz frequency range. According to a similar research made by Hemmati and the team, the remelting process consisted of a preheating step [11] with a velocity of the inductor relatively four-time faster than the one used for the remelting procedure.

Figure 2 presents the inductive remelting process of the NiCrBSi coating. The as-sprayed specimen was inserted in a copper coil, fixed in a lathe machine, which was continuously rotated. The induction coil was moving from right to left with a constant speed.



Figure 2
Inductive remelting process of the NiCrBSi coating

For further analysis, metallographic samples were prepared according to the standard guide for metallographic preparation of thermal sprayed coatings [15].

3 Results and Discussion

3.1 Morphology and Porosity of the NiCrBSi Coating

In the case of as-sprayed NiCrBSi coating presented in Figure 3, it can be remarked a network of interconnected porosity and unbound particles due to the impact, rebound and contraction of the particles, with the substrate during the deposition process. Nonetheless, taking into account the technological advances, the flame-sprayed NiCrBSi coatings contain unwanted oxides, show moderate adhesion to the substrate and contain a large amount of porosity [16].

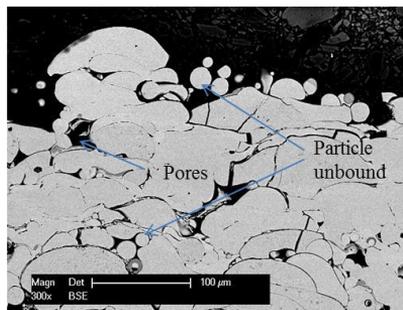


Figure 3

SEM micrograph of the as-sprayed NiCrBSi coating

The porosity degree was calculated with the aid of Leica QWin Image Processing and Analysis Software. The micrographs were acquired with an optical microscope and further processed. Figure 4 exhibits a considerably decrease of porosity from 15% in the case of as-sprayed coatings to a mean value of 1% after the flame remelting and respectively 0.5% after electromagnetic remelting treatment. The decrease of porosity in the case of the electromagnetic post-treatment can be caused by the capacity of the installation to control and set the temperature at a point close to the eutectic one where the wetting of the surface is done realizing a good gas extraction and a void closure.

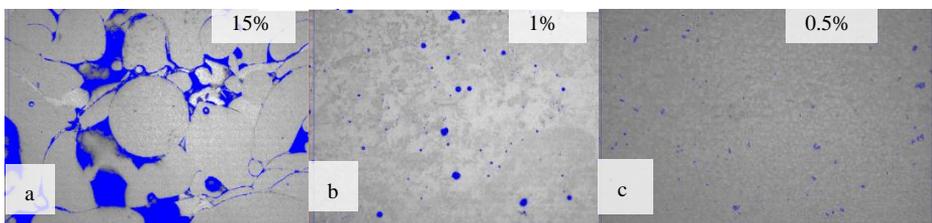


Figure 4

Optical micrographs of as-sprayed (a), flame remelted (b) and inductive remelted coatings (c)

The significant decrease of the porosity degree observed after the remelting process provides important information regarding the effectiveness of the post treatment, obtaining in this way a more compact NiCrBSi coating with a better adhesion to the substrate.

3.2 Microhardness and Tribological Behavior of the NiCrBSi Coating

Microhardness investigations were carried out on a Zwick Microhardness tester according to ISO 6507. The microhardness measurements were performed in 9 different spots along the cross-section of the NiCrBSi coating, the load used for determining the Vickers microhardness was 3 N applied for 15 seconds on each indentation and the distance between measurements was 0.15 mm. Figure 5 presents the values for the Vickers microhardness obtained for the NiCrBSi coating remelted by flame and respectively remelted using electromagnetic induction.

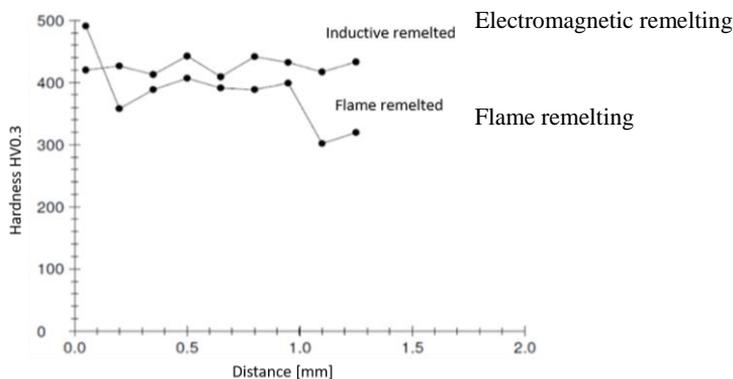


Figure 5

Microhardness values obtained for flame and electromagnetic remelted NiCrBSi coatings

A mean value of 390 HV0.3 was obtained for the flame remelted samples. For the electromagnetic fused samples 430 HV0.3 was measured with a smaller standard deviation, showing a homogenous coating along the surface. It is generally known that the hardness respectively the nanostructure of a material will directly influence its wear behavior [17]. Therefore, the sliding wear tests were performed using a pin-on-disc arrangement (POD) compliant to ASTM G99 and DIN 50324. This test design was chosen as the device is equipped with a friction coefficient transducer, providing on-line measurement of the friction coefficient. Testing parameters were maintained constant for all the samples: a counterbody of WC-Co, 6 mm diameter, 10 N load, linear speed of 15 cm s⁻¹ and 15000 laps (566 m).

Prior to the POD tests, all of the specimens were ground to a plane surface having the same roughness, cleaned with acetone and dried under warm air. The friction coefficient was continuously monitored during the tests. In this regard, the measured coefficients of the WC-Co ball against the coatings are presented in Figure 6.

For NiCrBSi coatings remelted by induction, the friction coefficient had a mean value of 0.603. Tribological tests concluded that the friction coefficient had a stable behavior, without fluctuations for the first 10000 laps and after that, it increased from 0.5 to 0.64 and stabilized at this value. The measurements showed that the NiCrBSi coating remelted by induction process exhibits a lower and steadier coefficient of friction in comparison with the flame remelted coating. The lower value of the friction coefficient obtained for the samples remelted by induction process, may be attributed to the lower porosity and a better adhesion between the particles of those samples, which leads to lower friction forces at the contact between sample and counterbody.

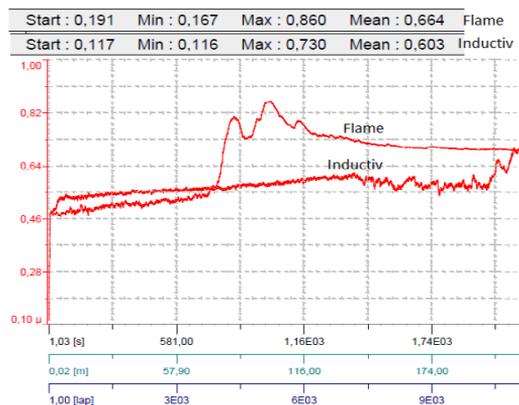


Figure 6

Friction coefficient of flame remelted and inductive remelted NiCrBSi coatings

After the test, the wear track investigations were performed on a confocal laser microscope, which facilitated the measurement of the depth of the tracks. The wear profiles of the NiCrBSi coating together with the mapping of the wear track are illustrated in Figure 7 and Figure 8.

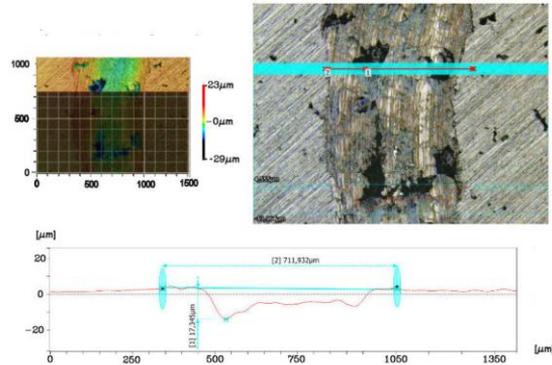


Figure 7

Wear track for sample remelted by flame

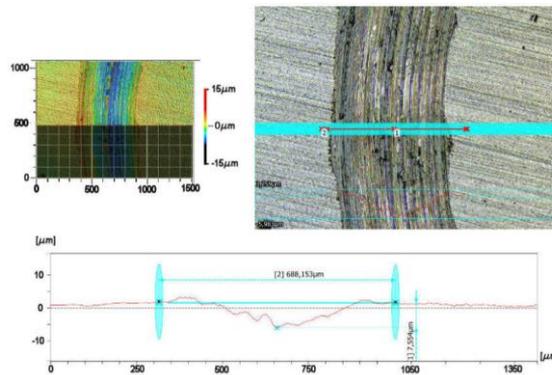


Figure 8

Wear track for sample remelted by inductive process

The wear rate calculated for induction remelted samples was $1.178 \cdot 10^{-4} \text{mm}^3 \text{N}^{-1} \text{m}^{-1}$ respectively $2.338 \cdot 10^{-4} \text{mm}^3 \text{N}^{-1} \text{m}^{-1}$ for the flame remelted ones. The obtained results demonstrate that a higher hardness of the tested surfaces leads in this situation to a lower material removal from the coating, giving a better resistance to wear in the case of induction remelted samples. In the previous figures one may observe that penetration depth of the ball was much lower for the inductively remelted coating ($7.5 \mu\text{m}$) for the inductive remelted coating respectively $17.3 \mu\text{m}$ for the flame fused coating).

3.3 Adhesive Properties

The adhesion to the substrate is one of the most important properties of the coated components. In order to determine if the coating has a good adhesion to the

substrate, the samples were investigated by realizing indentations on the substrate-coating interface.

The indentations were performed in different spots of the cross-section along the interface between the NiCrBSi coating and the substrate. The load used for examining the adhesion was 1200 N applied for 15 seconds on each test. In Fig. 9, before the remelting process, delamination, low mechanical bonding and cracks can be observed at the interface and in the coating. Figure 10 illustrates the indentations on both samples.

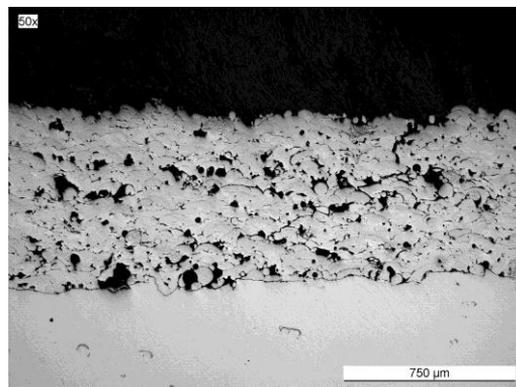


Figure 9

As-sprayed coating and interface overview

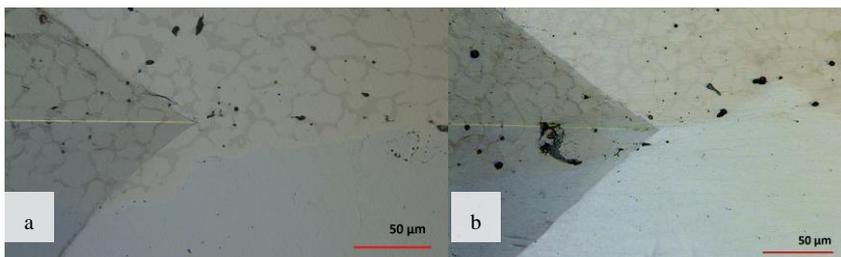


Figure 10

HV 120 indentation for flame (a) and inductive remelted coating (b)

The results show that both remelting processes offered a good adhesion to the substrate and delamination did not occur.

3.4 Corrosion Behavior

The corrosion behavior of the NiCrBSi coatings was investigated by electrochemical polarization in a three electrode cell in 3.5% NaCl aqueous solution. A saturated calomel electrode (SCE) was used as reference electrode, a

platinum electrode as auxiliary electrode and the NiCrBSi samples represented the working electrode. The samples were polarized in a potential interval from - 500 mV to +500 mV, with a scan rate of 0.16 mVs^{-1} .

Table 2
Corrosion potential and corrosion current densities of NiCrBSi coatings

Sample	$E_{\text{Corr vs SCE}} (i=0) [\text{mV}]$	$i_{\text{Corr}} [\text{mA cm}^{-2}]$
Flame	-268	$91 \cdot 10^{-4}$
Inductive	-217	$27 \cdot 10^{-4}$

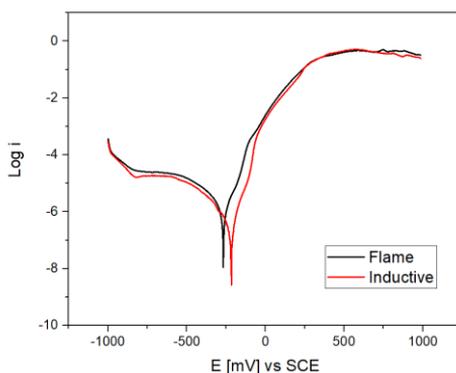


Figure 11

Polarization curves of the flame respectively inductively fused NiCrBSi coatings tested in 3.5% NaCl aqueous solution

It is important to mention that Bergant *et al.* have demonstrated in previous studies that the Ni-based treated coatings exhibit a better corrosion resistance with a factor of 10 compared to the substrate and the as-sprayed one [18]. Considering this data, the analyzed samples were the post-treated ones. The results presented in Table 2 and the polarization curves illustrated in Figure 11 reveal a higher corrosion rate for the NiCrBSi coating remelted by flame process compared to the inductive remelted one. As can be noticed, the corrosion current density i_{corr} is three times lower in the case of the inductive remelted sample ($\sim 27 \cdot 10^{-4} \text{ mA cm}^{-2}$) compare to the flame remelted one ($\sim 91 \cdot 10^{-4} \text{ mA cm}^{-2}$). The corrosion potential E_{corr} of the inductive post-treated sample which is slightly shifted to a positive value than the flame is another sign of superiority of the red marked coating. Regarding the anodic region of the graph, one can see that the curves present a similar behavior, presenting a slight repassivation plateau with an overlapping point at about 50 mV.

4 Conclusions

This work presents a new approach for obtaining NiCrBSi coatings with low porosity and good adhesion to substrate, using a two-step deposition process. As-sprayed, NiCrBSi coatings present high porosity, low cohesion between particles and poor adhesion to the substrate, as well as irregular surface geometry. The coatings which were remelted by induction are more compact and the porosity decreased with a factor of 30, from the as-sprayed one to the induction treated ones.

The microhardness investigations revealed that the inductive remelted NiCrBSi coatings do not present fluctuation of hardness and the mean value is 10% higher than the flame remelted ones. This fact can be attributed to a more compact microstructure with lower porosity, and a finer distribution of the phases.

Regarding the wear behavior, the wear rate of the electromagnetic samples was more than two times lower than the flame remelted one. The electrochemical corrosion tests showed that inductive remelted specimen, which is treated with a method that allows a precise control of the temperature and energy and exhibits a 3X better corrosion resistance than the flame remelted samples.

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